

(iii) and (iv)

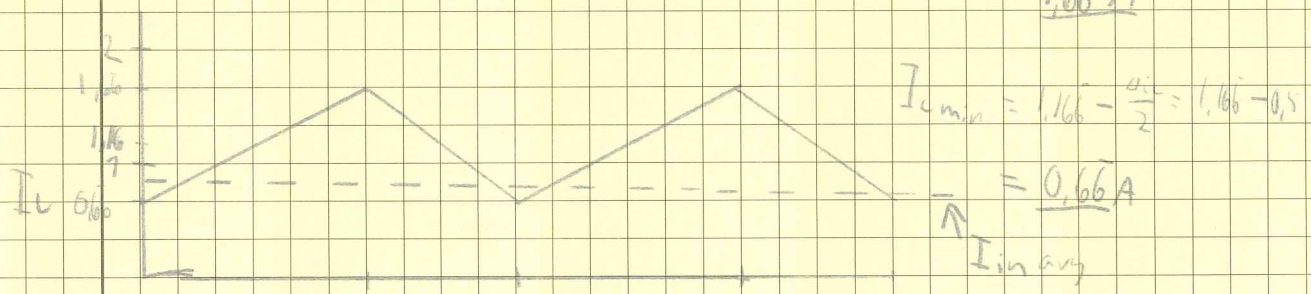
$$\Delta I_L = \frac{1}{L} D T_s \cdot (V_{in} - V_o) = \frac{1}{L} (1-D) T_s V_o$$

$$I_{in} = \frac{P_{in}}{V_{in}} = \frac{P_o}{V_{in}} = \frac{14}{20}$$

$$\Delta I_L = \frac{1}{24 \cdot 10^{-6}} \cdot 0,6 \cdot 5 \cdot 10^{-6} (20 - 12) = 7 \text{ A}$$

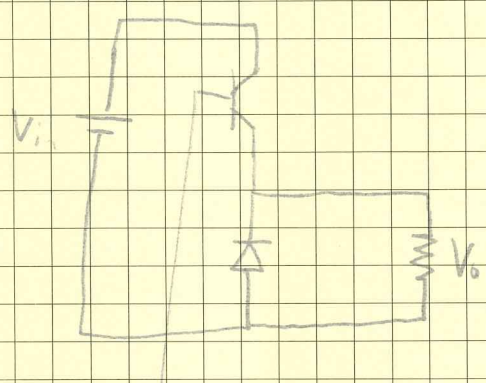
avg:  $I_L = I_o = \frac{P_o}{V_o} = \frac{14}{12} = 1,166$

$$I_{L_{max}} = 1,166 + \frac{\Delta I_L}{2} = 1,166 + 0,5 = 1,66 \text{ A}$$

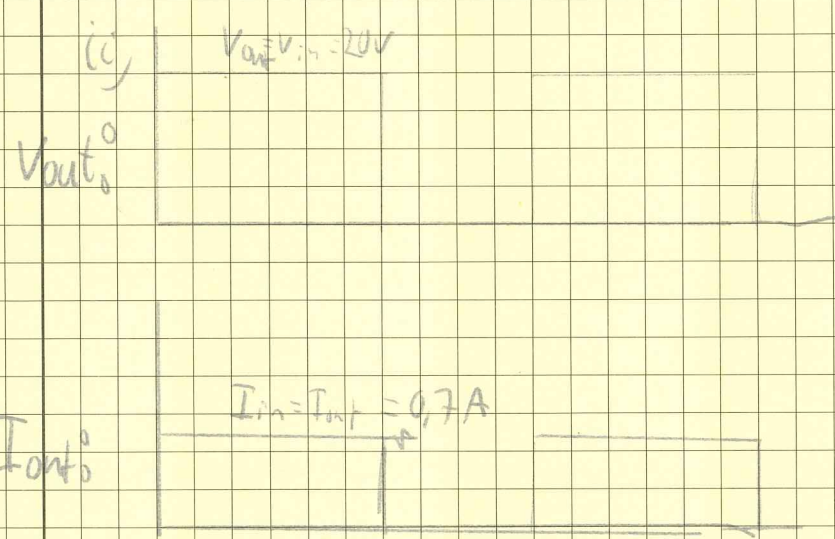




7  
b



i) The free-wheeling diode does nothing because when there is no inductor, there is no energy stored. So when the transistor is off, there is no power in the circuit.



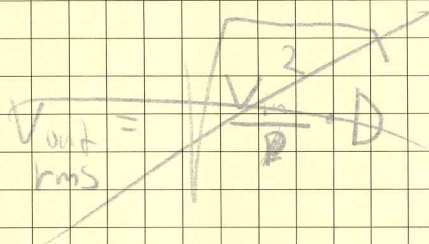
$$\bar{I}_{out} = I_{in} = \frac{P_o}{V_{in}} = \frac{14}{20} = 0,7$$

$$V_o \text{ avg} = \frac{V_{in} \cdot D + (1-D) \cdot 0}{1} = V_{in} \cdot D = \underline{12V}$$

$$I_o \text{ avg} = \frac{I_{in} \cdot D + (1-D) \cdot 0}{1} = I_{in} \cdot D = 0,7 \cdot 0,6 = \underline{0,42A}$$



b)  $i_v$ ,  $v_{rms}$ ;  $v_{out}$  mean square



root  $\cdot (V_{in} D)^2 \Rightarrow \text{mean } \frac{(V_{in} D)^2}{D}$   
square  $\Rightarrow \sqrt{\frac{V_{in}^2 D^2}{D}}$

$$V_{out\ rms} = \sqrt{\frac{(V_{in} D)^2}{D}}$$

$$= \sqrt{\frac{V_{in}^2 D^2}{D}} = \sqrt{V_{in}^2 D} = \underline{\underline{V_{in} \sqrt{D}}}$$

We know  $I = \frac{V}{Z}$  Since there is only R  $\Rightarrow I = \frac{V}{R}$

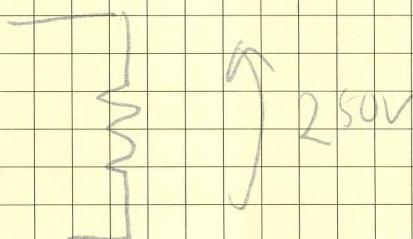
$$\underline{\underline{I = \frac{V_{in} \sqrt{D}}{R}}}$$



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$P_0 = 6250 \text{ kW}$

$PF = 0,5 \text{ lagr}$



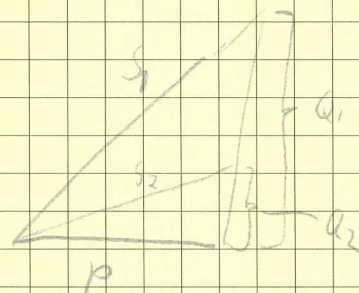
$S_1 = \frac{P}{\cos\phi} = \frac{6250 \text{ kW}}{0,5} = 12500 \text{ kVA}$

$Q_1 = \sqrt{S_1^2 - P^2} = \sqrt{12500^2 - 6250^2} = 10825,3 \text{ kVAr}$

$S_2 = \frac{P}{\cos\phi_2} = \frac{6250}{0,9} = 6944 \text{ VA}$

$Q_2 = \sqrt{S_2^2 - P^2} = 3027 \text{ kW}$

$Q_c = Q_1 - Q_2 = 10825 - 3027 = 7798 \text{ kVAr}$



$X_c = \frac{V^2}{Q_c} = \frac{250^2}{7798} = 8,101 \cdot 10^{-3}$

$X_c = \frac{1}{\omega C} \implies C = \frac{1}{\omega X_c} = \frac{1}{2\pi \cdot 50 \cdot 8,101 \cdot 10^{-3}} = 0,397 \text{ F}$

This was a very large capacitor.



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2-b) A capacitor in parallel makes the

load current less lagging, more leading.

An inductor does the opposite.

$$S = VI^* \quad * \text{conjugate.}$$

That means when I have negative angle. (lags)

the Q is positive.

Trigonometry shows us that  $P = VI \cos \theta$  (the real part of S)

and  $Q = VI \sin \theta$  (the imaginary part)

In this example the Power P stays the same,

~~that means~~ and Q is shrinking (getting smaller).

That means S also got smaller,  $\Rightarrow$  Since V is the same, and the angle of I got better (close to unity) this means |I| has to get smaller.

That is very good because the losses =  $I^2 R$



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3. a) We can not always measure all values of voltages, currents, and so on... in a system mostly because the measuring devices and machines are very expensive. It's quite easy to measure magnitudes of voltages and  $P$  and  $Q$  if we have ~~the~~ buses.

$P/Q$  bus - measures  $P$  and  $Q$

Slack bus - this is a "static bus" or reference

here we set the voltage to  $1 \text{ pu}$  and the angle to  $0^\circ$ .

Generator bus - here we have  $P$  and  $|V|$ .

we can choose  $Q$  to get these values

$(P/Q)$  bus

~~When we have~~

When we have the  $Y$  matrix it's very easy to calculate ~~the~~ currents etc.

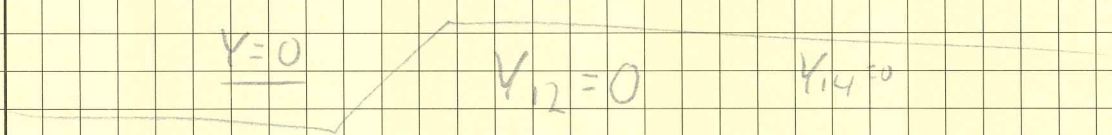
We use  $Y$  matrix because then we can solve by short circuiting other buses, ~~if we~~ to get the other voltages  $= 0$

when we have the  $Z$  matrix we need ~~the~~  $I_s$  to be  $0$  and it's more work to open/cut.



3<sub>g</sub> continues.

also the 2 broken buses who don't connect =  $\infty$



b)  $Z_{13} = (0,1 + j0,3)$   $Y_{13} = -\frac{1}{0,1 + j0,3} = -1 + 3i$

$Y_{multi} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} \end{bmatrix}$

$Z_{23} = -(0,5 + j0,4)$   $Y_{23} = -\frac{1}{0,5 + j0,4} = -0,66 + 2i$

$Z_{24} = -(0,1 + j0,3)$   $Y_{24} = \frac{1}{0,1 + j0,3} = -1 + 3i$

$Z_{34} = -(0,05 + j0,15)$   $Y_{34} = \frac{1}{0,05 + j0,15} = -2 + 6i$

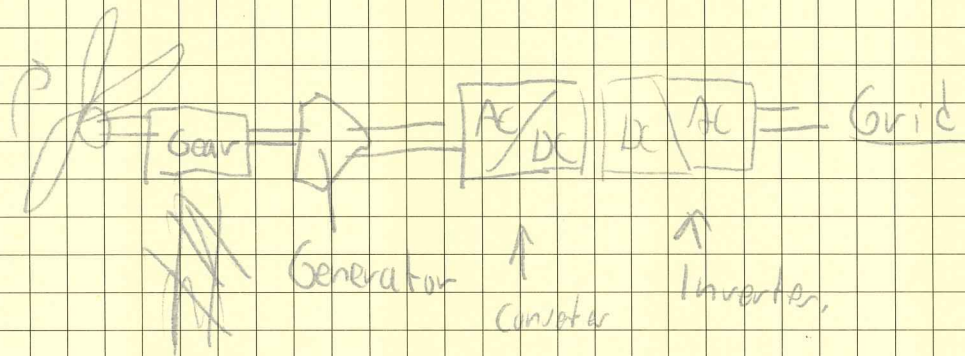
$Y = \begin{bmatrix} +1 + j3 & 0 & -1 + j3 & 0 \\ 0 & +1,66 - j5 & -0,66 + j2 & -1 + j3 \\ -1 + j3 & -0,66 + 2i & 3,66 - j11 & -2 + j6 \\ 0 & -1 + j3 & -2 + 6i & (3 - 9i) \end{bmatrix}$

$Y_{11} = -(Y_{12} + Y_{13} + Y_{14}) = -((1 + j3) + 0 + 0) = -1 - j3$

$Y_{21} = Y_{12} = 0$   $Y_{23} = Y_{32} = 0,66 - 2i$  /  $Y_{22} = -(Y_{21} + Y_{23} + Y_{24}) = -((0,66 - j2) + (1 + j3))$



4. b



Wind blows on the wings, the windmill has gears so that the rpm is higher, it needs to be when it comes to the generator, in the generator the mechanical power ~~is converted~~<sup>becomes</sup> AC power.

Because the AC power made by the generator ~~is~~ have very variable quality. It need to be converted to ~~be~~ Direct current. As we know the grid is AC, so the Direct current needs to be inverted back to AC. This time the AC is of much better quality, and can be feeded in to the grid.





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## 4c) Surge Impedance loading

The SIL is the border of loading which the line <sup>uses</sup> ~~delivers~~ more reactive effect ~~to~~ ~~the system~~ than it produces. The  $SIL = \frac{kV^2}{Z_c}$

$$\text{Where } Z_c = \sqrt{\frac{L}{C}}$$

The amount of reactive effect produced by line:  $\frac{kV^2}{X_c}$

The amount of reactive effect used by line:  $I^2 X_c$

$$\text{The border: } I^2 X_c - \frac{V^2}{X_c} = 0$$

↓

$$I^2 X_c = \frac{V^2}{X_c} \Rightarrow I^2_{WL} = \frac{V^2}{\frac{1}{\omega C}} = V^2 \omega C$$

$$I^2_{WL} = I^2 Z^2 \omega C \Rightarrow Z^2 = \frac{L}{C} \Rightarrow Z = \sqrt{\frac{L}{C}}$$

If the line is loaded above its SIL

It pulls Q from the system.  
(absorb)

If its loaded below its SIL it delivers Q to the system.



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4 d)

Load bus is a simple bus where  $P$  and  $Q$  is known.

Generator bus is a bus where  $P$  and  $|V|$  is known. in a generator bus we can adjust  $Q$  so that  $P$  and  $|V|$  should be same.

Slack bus is a bus taken as a ~~reference~~ <sup>reference</sup> where  $|V| = 1 pu$  and  $\angle V_{angle} = 0^\circ$

We have to have a reference bus or be able to calculate on the flow. therefore we take a "0" reference. It is not ~~in~~ <sup>real</sup>  $0^\circ$ , but we set it to be.

I explain more about bus in 3b)